

# Assessment of metal concentrations in tap-water – from source to the tap: a case study from Szczecin, Poland

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#### Abstract

The concentrations of Al, As, Cd, Cu, Pb, Zn, Ni, Fe and Mn were determined in June 2010 for 100 tap-water samples, collected directly at consumers in the older part of the city of Szczecin (Poland). Increased concentrations of metals were thus detected. This concerns mainly Fe (19% of samples showed concentrations above drinking-water quality standards) and Pb (5%). In some samples, the maximum admissible concentration levels for Mn, Cu and Ni were also exceeded. This was not the case for Al, despite the use of aluminium compounds during water treatment; the Al concentrations in treated water were, however, significantly higher than in raw water.

It was also found that (1) the corrosive properties of water (low alkalinity and increased concentration of sulphates), (2) the water-treatment processes causing a decrease of the pH and an increase of the  $CO_2$ , and (3) transport of the treated water over long distances (30 km) provide favourable conditions for the leaching of metals from water-pipe networks. The type of material used in domestic plumbing and the content of Ce, Fe, Mn, Ni and Cd in the tap-water at consumers show a correlation. The high content of Pb is mainly a result of lead pipes connecting the network to the buildings.

Keywords: chemical quality; water-distribution networks; metals; tap-water

# 1. Introduction

The 1998 EU Directive 98/83 EC Directive on drinking-water establishes strict standards, based on healthcare criteria, for metals (Sb, Cd, Cr, Cu, Pb, Hg, Ni) and metalloids (As, Se), as well as less strict standards for Al, Fe, Mn and Na. The directive also emphasises maintaining appropriate water quality at the final point of water-works: the consumers' taps. In view of the above directive, which has also been adopted by Polish law, it is crucial to study the changes of the chemical composition in water from the water-capture, through the treatment process and the distribution of treated water to consumers. Studies of changes in the water composition allow for designing activities which should be undertaken in order to obtain and maintain a water quality meeting the directive standards at the consumers.

According to the studies that have been conducted to date, the major problem for consumers is posed by the leaching of such metals as Pb, Cu and Ni from the distribution network and fittings (Schock, 1990; Smith, 1994; Sobesto, 1994; Toczyłowska, 1994; Al-Malack, 2001; Tamasi & Cini 2004; Karavoltsos et al., 2008; Veschetti et al., 2010, Turek et al., 2011, Górski & Siepak, 2011). The largest problem, however, is the leaching of lead, formerly used to manufacture the pipes. Moreover, components made of brass and soldering materials can also be a source of lead. According to data presented by Hayes et al. (2010), approx. 25% of the houses in the European Union may have lead installations, mainly in the form of pipes connecting the buildings to the network. In such buildings, the concentrations of lead may exceed 10  $\mu$ g L<sup>-1</sup>, which is the maximum admissible concentration in the EU (and also in Poland) since 2013.

In order to identify the above problem, analyses of metal concentration at consumers were conducted in Szczecin (NW Poland). The study area was the central part of the city, with old buildings fitted with lead pipes, in particular those connecting the buildings to the network. During the selection of the study area, factors favouring the leaching of metals from the distribution network were also taken into consideration: the corrosive properties of water (relatively low alkalinity and hardness of the raw water (which comes from Lake Miedwie) and the influence of aluminium sulphate, which is used during water treatment); the treated water is transported over 30 km through pipes made of iron.

consumers were conducted. It is one of the oldest and largest Polish cities. It is located in the north-western part of the country, in the province of Zachodniopomorskie, close to the Polish-German border (Fig. 1). The city covers an area of 301 km<sup>2</sup>, and has about 400,000 inhabitants (Dmochowska et al., 2010a,b). The city is divided into four quarters: Północ (North), Prawobrzeże (Right bank), Śródmieście (Centre) and Zachód (West).

The main source of water for the city is Lake Miedwie, located about 30 km south-east from the city centre (Fig. 1). It is a 16.2 km long and 3.2 km wide postglacial lake, with a surface area of 35.3 km<sup>2</sup> and a maximum depth of 43.8 m. The lake is located in a depression filled with silts, what hamper groundwater discharge to the lake. The water-capture facility, located along the lake with the water-treatment plant, produces about 85,000 m<sup>3</sup> of water daily, which constitutes about 90% of the city's water demand. The remaining 10% of the supply is covered by groundwater.

#### 1.2. Objectives

#### **1.1.** Selection of the study area

The city of Szczecin was selected as it is one of ten problem areas in Poland for which detailed studies of metal concentrations at the The study aimed to determine the influence of the above-mentioned factors favouring the leaching of metals from the water-distribution and water-transport networks on metal concentrations in consumers' tap-water in



Fig. 1. Location of the study area.

1 – zone supplied with water from the Miedwie Lake in the left-bank part of Szczecin; 2 – pumping station; 3 – water-production plant; 4 – area investigated in detail. Szczecin. The study was conducted as part of the 'Metals and related substances in drinking water in Poland' project, carried out within the Cost Action 637.

# 2. Materials and methods

### 2.1. Water-supply system

The water from Lake Miedwie is taken by the water-supply authorities from a depth of 16-18 m below the water surface, i.e. 6 m above the bottom of the lake. The water is then transported to the treatment plant, which is located 425 m away from the lake. The treatment involves preliminary oxidation using ozone, coagulation with aluminium sulphate, quick filtration through open filters, intermediate ozonisation, and adsorption on carbon filters. Disinfection is performed using chlorine dioxide. The treated water is transported to the city through a 15-km long pipeline with a diameter of 1200 mm, made of cast iron, then for another 15 km through a steel pipeline.

The total length of the pipeline network in Szczecin amounts to 1162 km. About 39% of the pipes in the distribution system are made of cast iron. The remaining pipes are made of steel (22%), PE (17%), PVC (11%), asbestos cement (3%), spheroid cast iron (2%) and other materials (6%). In the central part of the city, where the pipe network was constructed before 1900, the presence of lead pipes cannot be excluded, especially in the pipes connecting the buildings to the network.

#### 2.2. Characteristics of sampling points

The study was carried out in the city center (Fig. 1). In this area, samples for physical-chemical analysis were collected mainly from buildings older than 30 years with connection pipes of at least the same age. The buildings are mainly apartments (58% sampling points), and for the remaining part public buildings (29%) and detached houses (13%). The internal piping for water supply inside the buildings is 11-30 years old (62%) (Fig. 2). The connection



Fig. 2. Specification of the age of buildings, connection pipes, internal piping and taps of the sampling points in Szczecin (according to interviews with the householders).

pipes are mainly made of cast iron (56%), while pipes inside the buildings are mainly made of galvanised steel (43%) and copper (29%). In the buildings of less than ten years old, the pipes are mainly made of PVC (4%); in the buildings of over 30 years old, they are mainly made of galvanised steel (27%) and copper (19%). About half (52%) of the taps where tap-water was collected is not older than 10 years and they are mostly made of brass coated with chromium.

#### 2.3. Sample collection

The samples of tap-water were taken for chemical analysis in June 2010 using the random daytime sampling (RDT) method (Van den Hoven et al., 1999; Hoekstra et al., 2009). According to Hayes et al. (2010), this method, when applied to a large number of sampling points, allows for the identification of problems resulting from the leaching of metals from both distribution networks and domestic plumbing. The method involves collecting a water sample marked by a defined constant volume (1 litre) directly after opening the tap at a random time during the day. A total of 100 sites were sampled. The sampling covered 16 km<sup>2</sup> of the city centre divided into squares forming a grid of 400 x 400 m, with sampling points located in the centre of the squares.

From the 1 litre of water that was collected at each sampling site, two 100-mL samples that were to be used for the chemical analysis were stored in polyethene (HDPE) bottles produced

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by Nalgene<sup>®</sup>. The samples for the study of metals were preserved with 0.5 mL of 60% HNO<sub>3</sub> Ultrapur<sup>®</sup> (Merck, Darmstadt, Germany).

The pH, the electrolytic conductivity and the temperature of the water were determined in the samples at the sampling sites using a Multi 350i/SET (WTW, Weilheim, Germany) meter equipped with pH-Electrode SenTix 41 and TetraCon<sup>®</sup> 325 electrodes produced by WTW. During the sampling process, data concerning the materials used in the construction of the domestic plumbing and of the pipes connecting it to the network, as well as information about the age of the building and the installation, were recorded. After sampling, the samples were taken to the chemical laboratory in a mobile refrigerator at a temperature of  $4 \pm$ 2.5°C.

#### 2.4. Chemical analyses

Several techniques were used to determine the concentration of several elements in the water samples. For the determination of Al, As, Cd, Ni and Pb, inductively coupled plasma mass spectrometry (ICP-MS) was applied (XSeries II CCT spectrometer, Thermo Electron Corporation, UK). For the determination of Cu, Fe, Mn, Zn, Ca, Mg and Na, inductively coupled plasma optical emission spectrometry (ICP-OES) with a CID detector was used (IRIS Advantage Duo ER/S spectrometer, Thermo Jarrell Ash, USA). The determinations of Al, Cd, Cu, Pb, Zn, Ni, Fe and Mn in raw water were conducted using atomic absorption spectrometry in the Szczecin Waterworks Laboratory. The Cl<sup>-</sup> and SO<sub>4</sub><sup>2-</sup> concentrations were measured using ion chromatography (IC) with a Metrohm apparatus, model 881 Compact IC Pro (Metrohm AG, Herisau, Switzerland). Total alkalinity was measured by titration of a water sample against a methyl orange indicator. The operating conditions for ICP-MS, ICP-OES and IC analyses are listed in Tables 1 and 2.

Before the analysis, the samples were filtered through a filter with 0.45-µm pore diameter produced by Millipore (Billerica, MA, UAS) and Sartorius AG (Sartorius AG, Germany). During the chemical analysis, clean reagents for trace-element analysis and de-ionised water purified in equipment produced by Millipore (Billerica, MA, UAS) were used. CRM TMDA-51.3 (Environment Canada), SRM 1643e (National Institute of Standards & Technology, USA) and CRM RAIN-97 (Environ-

**Table 1.** Operating conditions for ICP-MS and ICP-OES determinations.

ICP-MS	
plasma torch	quartz, equipped with silver screen
nebulizer	glass concentric
R.F. frequency	27.12 MHz
forward power	1400 W
argon flow rates (L min <sup>-1</sup> ): - cool - auxiliary - nebulizer	13.0 0.72 0.95
target analyte isotopes monitored	<sup>27</sup> Al, <sup>75</sup> As, <sup>114</sup> Cd, <sup>60</sup> Ni, <sup>208</sup> Pb
internal standard	<sup>89</sup> Y
sample pumping flow rate (mL min <sup>-1</sup> )	approx. 0.8
uptake and wash times	60 s
$LOD (\mu g \cdot L^{-1})$	
Al	0.15
As	0.15
Cd	0.012
Ni	0.08
Pb	0.12
ICP-OES	
plasma torch	quartz, horizon- tal duo
plasma torch nebulizer	quartz, horizon- tal duo glass concentric
plasma torch nebulizer R.F. frequency	quartz, horizon- tal duo glass concentric 27.12 MHz
plasma torch nebulizer R.F. frequency forward power	quartz, horizon- tal duo glass concentric 27.12 MHz 1150 W
plasma torch nebulizer R.F. frequency forward power argon flow rates:	quartz, horizon- tal duo glass concentric 27.12 MHz 1150 W
plasma torch nebulizer R.F. frequency forward power argon flow rates: – plasma (L min <sup>-1</sup> )	quartz, horizon- tal duo glass concentric 27.12 MHz 1150 W 15
plasma torch nebulizer R.F. frequency forward power argon flow rates: - plasma (L min <sup>-1</sup> ) - intermediate (L min <sup>-1</sup> )	quartz, horizon- tal duo glass concentric 27.12 MHz 1150 W 15 15
plasma torch nebulizer R.F. frequency forward power argon flow rates: - plasma (L min <sup>-1</sup> ) - intermediate (L min <sup>-1</sup> ) - optics interface (L min <sup>-1</sup> )	quartz, horizon tal duo glass concentric 27.12 MHz 1150 W 15 1 4
plasma torch nebulizer R.F. frequency forward power argon flow rates: - plasma (L min <sup>-1</sup> ) - intermediate (L min <sup>-1</sup> ) - optics interface (L min <sup>-1</sup> ) - purging optics (L min <sup>-1</sup> )	quartz, horizon tal duo glass concentric 27.12 MHz 1150 W 15 1 1 4 4 20
plasma torch nebulizer R.F. frequency forward power argon flow rates: - plasma (L min <sup>-1</sup> ) - intermediate (L min <sup>-1</sup> ) - optics interface (L min <sup>-1</sup> ) - purging optics (L min <sup>-1</sup> ) - purging CID detector (units)	quartz, horizon tal duo glass concentric 27.12 MHz 1150 W 15 1 1 4 4 4 80
plasma torch nebulizer R.F. frequency forward power argon flow rates: - plasma (L min <sup>-1</sup> ) - intermediate (L min <sup>-1</sup> ) - optics interface (L min <sup>-1</sup> ) - purging optics (L min <sup>-1</sup> ) - purging CID detector (units) - nebulizer pressure (psi)	quartz, horizon- tal duo glass concentric 27.12 MHz 1150 W 15 1 4 4 4 80 26
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plasma torch nebulizer R.F. frequency forward power argon flow rates: - plasma (L min <sup>-1</sup> ) - intermediate (L min <sup>-1</sup> ) - optics interface (L min <sup>-1</sup> ) - optics interface (L min <sup>-1</sup> ) - purging optics (L min <sup>-1</sup> ) - purging optics (L min <sup>-1</sup> ) - purging CID detector (units) - nebulizer pressure (psi) sample pumping flow rate (mL min <sup>-1</sup> ) rinsing time LOD (μg·L <sup>-1</sup> ) Cu Zn	quartz, horizon tal duo glass concentric 27.12 MHz 1150 W 15 1 4 4 80 26 30 26 30 26 30 50 30 30 30 30 30 30 30 30 30 30 30 30 30
plasma torch nebulizer R.F. frequency forward power argon flow rates: - plasma (L min <sup>-1</sup> ) - intermediate (L min <sup>-1</sup> ) - optics interface (L min <sup>-1</sup> ) - purging optics (L min <sup>-1</sup> ) - purging optics (L min <sup>-1</sup> ) - purging CID detector (units) - nebulizer pressure (psi) sample pumping flow rate (mL min <sup>-1</sup> ) rinsing time LOD (μg·L <sup>-1</sup> ) Cu Zn Fe Mn Ca	quartz, horizon, tal duo   glass concentric   27.12 MHz   1150 W   1   1   1   1   1   1   1   1   4   4   80   26   approx.2   60 s   1.5   0.49   0.71   0.19   70
plasma torch nebulizer R.F. frequency forward power argon flow rates: - plasma (L min <sup>-1</sup> ) - intermediate (L min <sup>-1</sup> ) - optics interface (L min <sup>-1</sup> ) - purging optics (L min <sup>-1</sup> ) - purging OID detector (units) - nebulizer pressure (psi) sample pumping flow rate (mL min <sup>-1</sup> ) rinsing time LOD (μg·L <sup>-1</sup> ) Cu Zn Fe Mn Ca	۹     quartz, horizon tal duo     glass concentric     27.12 MHz     1150 W     1     1     1     1     1     1     1     1     1     1     4     4     80     26     300 26     200 26     300 26

Analyse	Analytical parameters	Element	LOD [mg·L <sup>-1</sup> ]
anions	Metrosep A Supp 5-150/4.0 column Metrosep A Supp 4/5 Guard/4.0 sequential suppression system: chemical suppressor MSM II and MCS	Cl-	0.011
	suppressor CO <sub>2</sub> conductivity detection eluent: 3.2 mmol L <sup>-1</sup> Na <sub>2</sub> CO <sub>3</sub> /1.0 mmol L <sup>-1</sup> NaHCO <sub>3</sub> , flow rate 0.7 μL min <sup>-1</sup>	SO42-	0.02

Table 2. General conditions and parameters of the analytical technique (IC).

ment Canada) were used as certified reference materials.

# 3. Results

#### 3.1. Quality of raw and treated water

The water taken from Lake Miedwie is characterised by a relatively low alkalinity and hardness. The concentrations of sulphates and, to a lower extent, of chlorides are relatively high. The metal concentrations are low, far below the admissible level in water meant for consumption, following the national Polish standards (PMH, 2010) and the European Directive (EC, 1998). During the water treatment, the concentrations of Mn, Cu, Fe, and Zn decrease, while the concentration of Al increased significantly, which may be ascribed to coagulation with aluminium sulphate. The concentration of aggressive CO<sub>2</sub> also goes up during the treatment, as a result of  $Al_2(SO_4)_3$ hydrolysis and the formation of H<sub>2</sub>SO<sub>4</sub>. Simultaneously the pH and alkalinity of the water decrease, which causes its corrosive properties (Rybicki, 2011). The corrosive properties of the treated water reach a value of 2.1 according to the Larson-Skold index (Larson & Skold 1958), indicating its corrosive character. It should be emphasised, however, that the treated water meets the Polish and the European Union standards for drinking water (Table 3).

#### 3.2. Quality of the tap-water

In the water collected at consumers, the pH ranged from 7.46 to 8.07, and the electrolytic conductivity from 600 to 672  $\mu$ S cm<sup>-1</sup>. The concentration of calcium was from 70.0 to 87.0 mg L<sup>-1</sup>, magnesium from 12.8 to 17.3 mg L<sup>-1</sup>,

sodium from 21.7 to 27.9 mg  $L^{-1}$  and chlorides from 47.6 to 66.6 mg  $L^{-1}$ . The concentrations of sulphates (117.9–121.4 mg  $L^{-1}$ ) and alkalinity (3.0–3.5 meq  $L^{-1}$ ) were slightly higher in the water at consumers than in the treated water (Table 3). The temperature of the water collected from the taps was also higher, which is relevant because a higher water temperature may accelerate the leaching of metals from the water pipe networks, as observed by Koh et al. (1991) and Al-Malack (2001).

The study of the metal contents at the consumers showed significantly higher concentrations of most metals than the treated water (Table 3), which must be ascribed to the leaching from the water pipe network. The increase concerned particularly Fe, Zn and Cu, as well as Mn and Cd. Leaching from the network was indicated for Pb and Ni by maximum values, higher than those observed in the raw and the treated water. As a result of the increased metal concentrations in the tap-water at consumers, these concentrations sometimes exceed the admissible values for drinking water. This concerns Fe (19% of the analyses), Pb (5%), Ni (1%), Mn (1%) and Cu (1%) (Fig. 3). The study also showed that the Al concentration in the water at consumers is higher than in the raw water of Lake Miedwie. This increase is due to the coagulation with  $Al_2(SO_4)_3$ . The maximum concentrations do, however, not exceed the admissible values (Fig. 3).

# 4. Discussion regarding the threat to consumers

The main threat to consumers is the occurrence of lead in concentrations which exceed the admissible values (5% of the cases). The lead pipes in the water pipe network are the most likely Pb source in the tap-water. Nev-

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Table 3. Statistical value	of phys	sico-che	mical pa	rameters	of raw v	vater, tre	ated wat	ter and w	vater sam	iples col	lected a	t consum	ners.				
		ł	law watu	er			Tre	ated wat	er		Dr	inking v	vater at c	onsumer	S	Drinkin ter guid	g-wa- elines
parameters	min.	max.	aver- age	SD	ч	min.	max.	aver- age	SD	E	min.	max.	aver- age	SD	я	EU (98/ 83/ EC)	per- cent- age of ex- cess
temperature (°C)	1.10	13.0	5.87	3.00	C Li	3.10	12.7	7.99	0.94	101	14.3	24.0	18.0	1.85		* * '	
Hd	7.50	8.50	8.00	0.25	CC7	7.30	7.90	7.58	0.12	104	7.46	8.07	7.63	0.08	001	6.5-9.5	0
conductivity (µS cm <sup>-1</sup> )	586	646	630	18.1	10	627	649	643	1.00	ы	600	672	623	7.32	TUU	2,500	0
alkalinity (meq $L^{-1}$ )	2.5	2.9	2.7	0.12	Ľ	1.3	2.8	2.6	0.19	104	3.0	3.5	3.2	0.20		**	
$Ca^{2+}$ (mg $L^{-1}$ )	62.4	76.4	69.7	3.05	10	62.5	75.3	69.69	2.45	21	70.0	87.0	73.7	7.02		* * '	
$Mg^{2^{+}}$ (mg $L^{-1}$ )	*,	*,	*	I		*,	*,	*,	ı		12.8	17.3	16.1	1.82		**	
Na <sup>+</sup> (mg L <sup>-1</sup> )	*,	*,	*,	,		*,	*,	*,	ı		21.7	27.9	26.3	2.56	10	200	0
Cl- (mg L <sup>-1</sup> )	47.5	51.8	49.1	1.03	51	51.8	56.0	54.1	0.78	21	47.6	66.6	61.0	7.29		250	0
SO <sub>4</sub> <sup>2-</sup> (mg L <sup>-1</sup> )	67.5	101.6	93.5	6.19	40	86.4	98.3	93.1	3.19	19	117.9	121.4	119.1	0.94		250	0
Al (μg ·L <sup>-1</sup> )	<0.1	12.0	5.60	4.00	51	<0.2	24	11.3	4.64	103	3.77	95.6	15.8	9.73		200	0
As (µg L <sup>-1</sup> )	*,	*,	*,	ı		*,	*,	*,	ı		0.15	0.91	0.55	0.12		10	0
Cd (μg Ł <sup>-1</sup> )	<0.1	0.10	0.03	0.09		<0.1	0.10	0.03	0.09		0.01	1.75	0.05	0.24		Ŋ	0
Cu (μg Ł <sup>-1</sup> )	1.00	34.0	13.0	0.02		1.0	19.0	12.0	2.01		1.50	2240	22.4	271.2		2,000	1
Pb (μg L <sup>-1</sup> )	<0.1	2.00	1.00	1.00	С	*,	*,	*,	ı	ю	0.12	22.1	0.84	3.52	100	10	Ŋ
Zn (µg L <sup>-1</sup> )	<0.1	7.00	3.00	4.00		0.7	35.0	12.7	3.25		11.9	2790	135.2	384.1		* * 1	
Ni ( $\mu g \cdot L^{-1}$ )	<0.1	5.00	2.00	3.00		*, 1	*ı	*,	ı		0.79	65.3	1.49	6.63		20	1
Fe (μg ·L <sup>-1</sup> )	<0.8	45.0	19.0	11.5	ŭ	<0.8	10	2.43	1.93	10	22.1	2870	105.5	302.8		200	19
Mn ( $\mu g \cdot L^{-1}$ )	<0.5	20.0	10.0	3.15	71	<0.5	10	1.90	3.75	17	0.96	98.0	5.47	11.6		50	2
-* = not determined -** = unlimited																	



**Fig. 3.** Metal concentrations in tap water in Szczecin obtained using the random daytime method. NDS: above acceptable levels in drinking water.

ertheless, the average concentration of lead in the tap-water is low and in 90% of the samples it does not exceed 5  $\mu$ g L<sup>-1</sup>. The maximum lead concentration is 22.1  $\mu$ g L<sup>-1</sup>. Although the concentration of lead indicates a medium risk according to the classification of Hayes et al. (2010), it requires certain action in order to minimise this threat.

The most exceeded admissible values concern Fe (19%). This is a significant threat for the water consumers and requires remedial action (Hayes et al., 2010). The cause of the exceeded values is the leaching of Fe during the long-distance transportation of water over 30 km in steel and cast-iron pipes, as well as the leaching of Fe from domestic plumbing, especially if constructed from galvanised steel pipes (Fig. 4). It should be underlined that ferruginous deposits formed as a result of the corrosion of steel pipes may provoke the leaching of lead from pipes made of this material (Hayes et al., 2010).

The threat to the consumers due to the concentrations of Ni, Cu and Mn is very low. Only single cases of exceeded admissible concentrations were found. In the case of Cu, this concerns a building with an installation made of copper, and in the case of Ni and Mn installations of galvanised steel were responsible. The admissible values are not exceeded for As and Cd. However, intensive leaching of Zn from the water pipe network takes place. The maximum concentration of this metal amounts to  $2790 \ \mu g \ L^{-1}$ .

The type of material used in domestic plumbing appears correlatable with the metal concentrations in the tap-water (Fig. 4). In particular, higher concentrations of Fe, Mn, Cd and Ni were found in the tap-water of apartments with plumbing made of galvanised steel pipes and copper pipes, which has also been reported by Smith (1994) and Toczyłowska (1994). Slightly higher Pb concentrations were also found in the apartments with galvanised steel pipes (Fig. 4). However, the differences between the analysed installation types are minor, which suggests that the pipes made of lead in the water pipe network are the main source of this metal, which was also noticed by Cheng & Foland (2005). A certain influence of PVC pipes plasticised with lead is also possible, as noted earlier by Koh et al. (1991) and Al-Malack (2001). It is worth mentioning here that no significant differences in Zn concentrations for particular installation types were found, which might indicate that the main source of this metal are taps, along with the connections to the pipe.





# 5. Conclusions

The study of water at consumers in Szczecin using the RDT sampling method indicated higher metal concentrations than in raw and treated water. This concerns especially Fe, Zn and Cu, and to a lesser extent Mn and Cd. In the case of Pb and Ni, higher maximum concentrations were found, which do not occur in raw and treated water. The study shows very low concentrations of As and their minor distribution, which does indicate the absence of leaching of this metalloid from the distribution network. For Al, a significant increase in concentration was found in treated water, which results from the application of coagulation with aluminium sulphate. A certain increase in concentration was also found at consumers. However, due to the lack of network elements constructed from this metal, this phenomenon should be linked to the leaching of Al from sediments accumulated in the network.

The significant increase of the Fe concentration should be ascribed mainly to the leaching of this metal from the water-distribution network between the water-treatment station and consumers over a distance of more than 30 km. The high Pb concentration, exceeding the admissible standard, should in turn be linked to the leaching of this element from lead pipes connecting the network to the buildings, which conclusion must be drawn on the basis of the information obtained from the residents. The leaching of Cu and, to a certain extent, of Ni, Mn and Cd occurs mainly in the internal plumbing system, as a high Cu concentration was found in installations made of copper, whereas increased Fe, Ni, Cd concentrations and, to a lesser extent, Mn concentrations occur in installations made of galvanised steel pipes.

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